

# DESIGN CALCULATION

LMTD

# A Methodology for Heat Exchanger Design Calculations

- The Log Mean Temperature Difference (LMTD) Method -

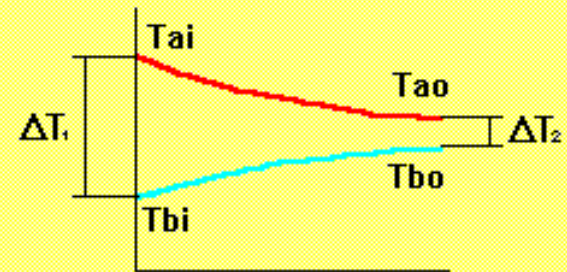
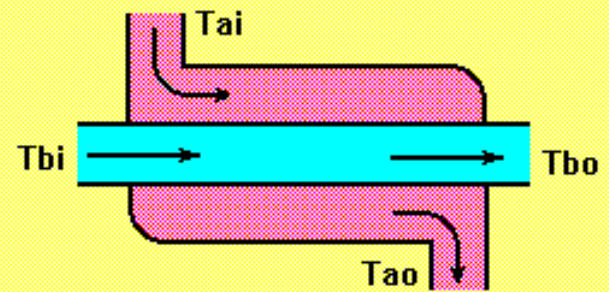
- A form of Newton's Law of Cooling may be applied to heat exchangers by using a log-mean value of the temperature difference between the two fluids:

$$q = U A \Delta T_{1m}$$
$$\Delta T_{1m} = \frac{\Delta T_1 - \Delta T_2}{\ln(\Delta T_1 / \Delta T_2)}$$

Evaluation of  $\Delta T_1$  and  $\Delta T_2$  depends on the heat exchanger type.

# Koefisien Transfer Panas Menyeluruh (U)

$$U = \frac{1}{\frac{1}{h_1} + \frac{\Delta x}{k} + \frac{1}{h_2}}$$



Temperature distribution along tube axis.

# TEMPERATURE terms

- **Approach temp. :**

temperature difference in one terminal (inlet / outlet)

Batasan umum :

$\Delta T$  app. : 10-20 F utk suhu ambient hingga 300 F

1-2 F atau  $< 10$  F utk cryogenic &  $<$  ambient

$\sim 100$  F utk suhu tinggi

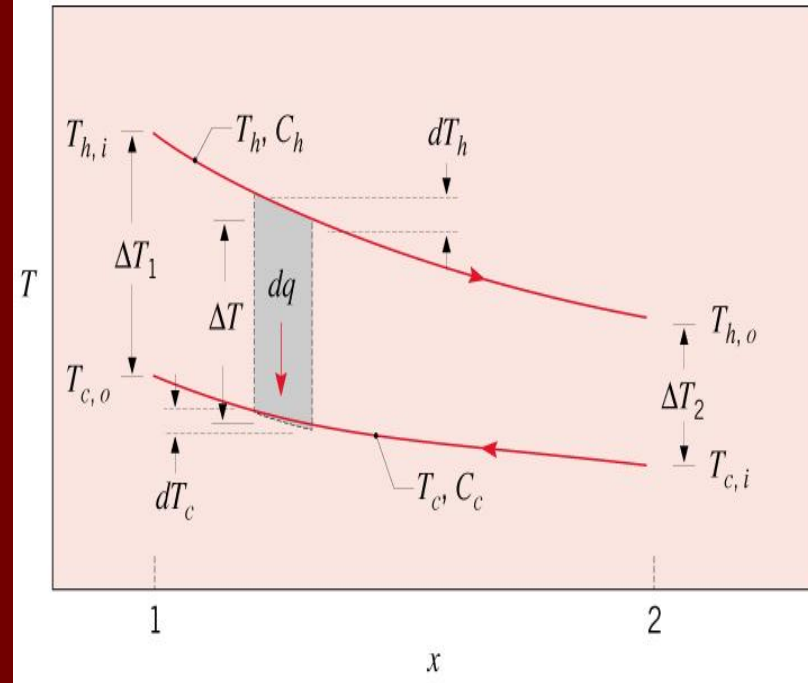
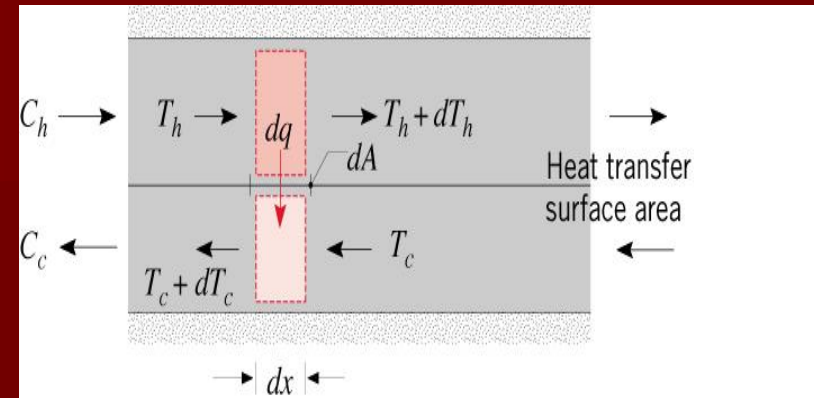
- **Range temp. :**

the actual temp. rise / fall

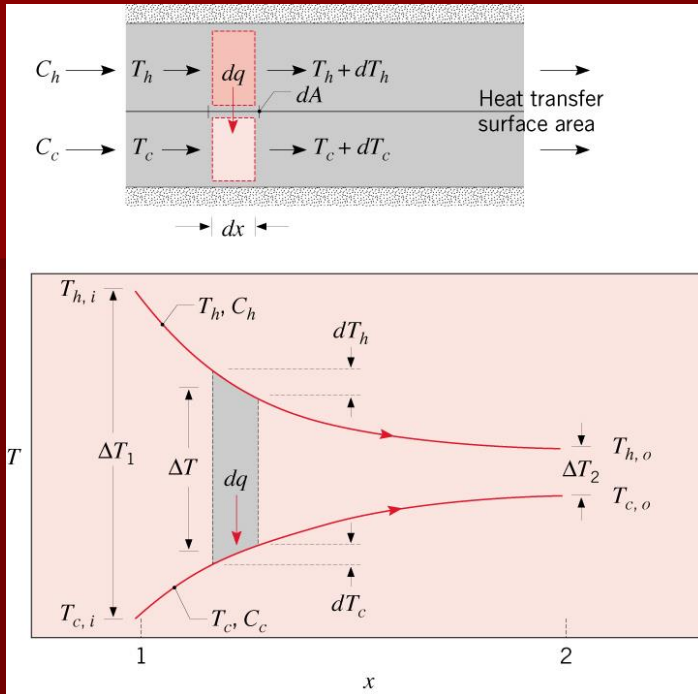
- Counter-Flow Heat Exchanger:

$$\begin{aligned}\Delta T_1 &\equiv T_{h,1} - T_{c,1} \\ &= T_{h,i} - T_{c,o}\end{aligned}$$

$$\begin{aligned}\Delta T_2 &\equiv T_{h,2} - T_{c,2} \\ &= T_{h,o} - T_{c,i}\end{aligned}$$



- Parallel-Flow Heat Exchanger:



$$\begin{aligned} \Delta T_1 &\equiv T_{h,1} - T_{c,1} \\ &= T_{h,i} - T_{c,i} \end{aligned}$$

$$\begin{aligned} \Delta T_2 &\equiv T_{h,2} - T_{c,2} \\ &= T_{h,o} - T_{c,o} \end{aligned}$$

- Note that  $T_{c,o}$  can not exceed  $T_{h,o}$  for a PF HX, but can do so for a CF HX.
- For equivalent values of  $UA$  and inlet temperatures,

$$\Delta T_{1m,CF} > \Delta T_{1m,PF}$$

# Soal 1

- Fluida panas memasuki pipa konsentris pada suhu 300 F dan didinginkan hingga 200 F menggunakan fluida dingin yg masuk pada suhu 100 F dan keluar bersuhu 150 F.
  - a. Berapa nilai  $\Delta T$  lmtd ?
  - b. Susunan mana yg lebih baik, paralel atau lawan arah ?

# Soal 2

- Diinginkan untuk memanaskan 9820 lb / hr benzene dari suhu 80 F menjadi 120 F, menggunakan toluen panas bersuhu 160 F yang akan mendingin menjadi 100 F.
  - A. Berapa laju alir toluen yang dibutuhkan untuk keperluan ini ?
  - B. Bila nilai  $U = 115 \text{ Btu/hr.ft}^2.\text{F}$ , berapa luas transfer panas yg diperlukan?
  - C. Jenis HE apa yang sesuai ?



# Soal 3

- Diinginkan untuk mendinginkan 33114 lb / hr butanol dari suhu 210 F menjadi 105 F, menggunakan air bersuhu 95 F yang akan memanaskan menjadi 105 F.
  - A. Berapa laju alir air yang dibutuhkan untuk keperluan ini ?
  - B. Bila nilai  $U = 200 \text{ Btu/hr.ft}^2.\text{F}$ , berapa luas transfer panas yg diperlukan?
  - C. Jenis HE apa yang sesuai ?

- Shell-and-Tube and Cross-Flow Heat Exchangers:

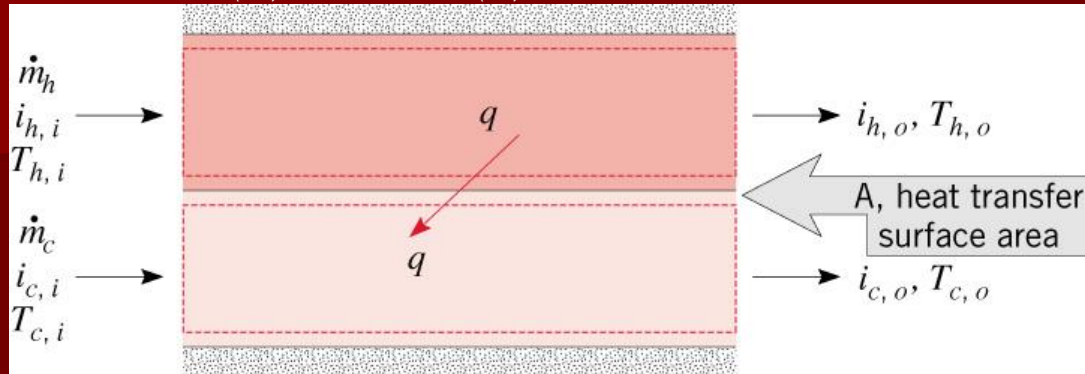
$$\Delta T_{1m} = F \Delta T_{1m,CF}$$



Grafik F di Kern utk  
berbagai susunan HE  
(fig.18-23 Appendix)

# Overall Energy Balance

- Application to the *hot (h)* and *cold (c)* fluids:



- Assume negligible heat transfer between the exchanger and its surroundings and negligible potential and kinetic energy changes for each fluid.

$$q = \dot{m}_h (i_{h,i} - i_{h,o})$$

$$q = \dot{m}_c (i_{c,o} - i_{c,i})$$

$i \rightarrow$  fluid enthalpy

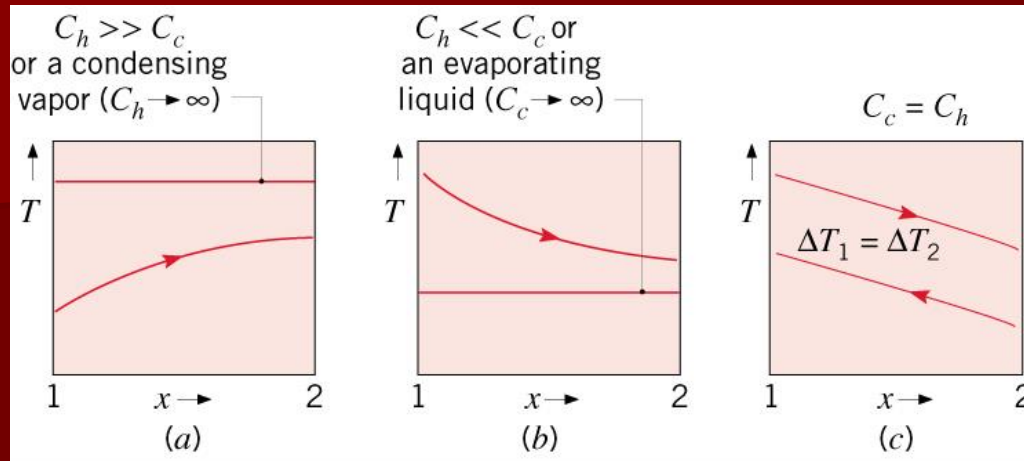
- Assuming no  $l/v$  phase change and constant specific heats,

$$q = \dot{m}_h c_{p,h} (T_{h,i} - T_{h,o}) = C_h (T_{h,i} - T_{h,o})$$

$$q = \dot{m}_c c_{p,c} (T_{c,o} - T_{c,i}) = C_c (T_{c,o} - T_{c,i})$$

$C_h, C_c \rightarrow$  Heat capacity rates

# Special Operating Conditions



- Case (a):  $C_h \gg C_c$  or  $h$  is a condensing vapor ( $C_h \rightarrow \infty$ ).
  - Negligible or no change in  $T_h$  ( $T_{h,o} = T_{h,i}$ ).
- Case (b):  $C_c \gg C_h$  or  $c$  is an evaporating liquid ( $C_c \rightarrow \infty$ ).
  - Negligible or no change in  $T_c$  ( $T_{c,o} = T_{c,i}$ ).
- Case (c):  $C_h = C_c$ .

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$$\Delta T_1 = \Delta T_2 = \Delta T_{1m}$$

# Tahapan perancangan HE

- Menentukan beban panas
  - kec. Transfer panas ( $q$ )
  - kec. Alir massa ( $m$ )
  - suhu
- Menentukan sifat fisis fluida (panas / dingin) :  $\mu$ ,  $\rho$ ,  $C_p$ ,  $k$ , dll
- Mengestimasi nilai  $U_D$
- Menghitung nilai  $\Delta T$ ,  $A$  (dari pers.  $Q = UA \Delta T$ )

# Cont'd

- Menentukan jenis HE (DPHE < 200 ft<sup>2</sup>)
- Menentukan panjang pipa (L), jumlah tube (Nt), ID, OD, BWG (tebal pipa, Birmingham Wire Gauge)
- Menentukan lay out pipa (jenis pitch & P<sub>T</sub>)
- Menghitung h<sub>i</sub>, h<sub>o</sub>, h<sub>io</sub> (h<sub>io</sub> = h<sub>i</sub> \* (ID/OD))
- Menghitung U<sub>c</sub> dan R<sub>d</sub>  
U<sub>c</sub> = (h<sub>io</sub>.h<sub>o</sub>)/(h<sub>io</sub>+h<sub>o</sub>)  
R<sub>d</sub> = (U<sub>c</sub>-U<sub>d</sub>)/(U<sub>c</sub>.U<sub>d</sub>)
- \* Menghitung pressure drop (Δp) pipa & shell

# Pertimbangan desain

- Penempatan fluida

- tubes :

- utk fluida yang korosif, *fouling*, *hazardous*, *scaling*,  
*bertekanan tinggi*, *bersuhu tinggi*, *bernilai tinggi (mahal)*

*OD <<, Δp >> → fouling terjadi lebih cepat*

*OD >>, v <<, Re << → h <<*

*triangular pitch : turbulensi >> → h >>, Δp >>*

*square pitch : turbulensi << → h <<, Δp <<*

- D tubes umumnya : 5/8 " – 1/12 "
- Panjang tubes : 6, 8, 12, 16, 20 ft
- Jumlah pass : 1 - 16



- shell :

utk fluida yang lebih viskos, lebih bersih,  
flow rate rendah, serta *evaporating &*  
*condensing fluids*

baffle → meningkatkan turbulensi ( $h_o \gg$ )

tinggi baffle umumnya 75% ID shell

B :  $(1/5 - 1) \cdot \text{ID shell}$